### **STORMWATER CALCULATIONS**

### Vertex Rail and Site Improvements Phase 1

**Vertex Property** 

Vertex Railcar Corporation 202 Raleigh Street Wilmington, NC 28412

October 2015



Daniel E. Dawson, PE
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NC License No. F-0374

Permit No	
	(to be provided by DWQ)

### STORMWATER MANAGEMENT PERMIT APPLICATION FORM 401 CERTIFICATION APPLICATION FORM

### WET DETENTION BASIN SUPPLEMENT

This form must be filled out, printed and submitted.

The Required Items Checklist (Part III) must be printed, filled out and submitted along with all of the required information.

I. PROJECT INFORMATION		
Project name	Vertex Rail and Site Improve	ments Phase 1
Contact person	Daniel E. Dawson, PE	
Phone number	910.762.4200	
Date	10/1/2015	
Drainage area number	1	
II. DESIGN INFORMATION		
Site Characteristics		
Drainage area	453,250 ft <sup>2</sup>	
Impervious area, post-development	263,793 ft <sup>2</sup>	
% impervious	58.20 %	
Design rainfall depth	1.5 in	
Storage Volume: Non-SA Waters		
Minimum volume required	32,510 ft <sup>3</sup>	OK
Volume provided	33,134 ft <sup>3</sup>	OK, volume provided is equal to or in excess of volume required.
Storage Volume: SA Waters		
1.5" runoff volume	ft <sup>3</sup>	
Pre-development 1-yr, 24-hr runoff	ft <sup>3</sup>	
Post-development 1-yr, 24-hr runoff	ft <sup>3</sup>	
Minimum volume required	ft <sup>3</sup>	
Volume provided	ft <sup>3</sup>	
Peak Flow Calculations		
Is the pre/post control of the 1yr 24hr storm peak flow required?	Y (Y or N)	
1-yr, 24-hr rainfall depth	3.86 in	
Rational C, pre-development	N/A (unitless)	
Rational C, post-development	(unitless)	
Rainfall intensity: 1-yr, 24-hr storm	in/hr	
Pre-development 1-yr, 24-hr peak flow	25.66 ft <sup>3</sup> /sec	
Post-development 1-yr, 24-hr peak flow	26.61 ft <sup>3</sup> /sec	
Pre/Post 1-yr, 24-hr peak flow control	0.95 ft <sup>3</sup> /sec	
Elevations		
Temporary pool elevation	41.40 fmsl	
Permanent pool elevation	40.20 fmsl	
SHWT elevation (approx. at the perm. pool elevation)	40.20 fmsl	
Top of 10ft vegetated shelf elevation	40.70 fmsl	
Bottom of 10ft vegetated shelf elevation	39.70 fmsl	
Sediment cleanout, top elevation (bottom of pond)	34.00 fmsl	
Sediment cleanout, bottom elevation	33.00 fmsl	
Sediment storage provided	1.00 ft	
Is there additional volume stored above the state-required temp. pool?	N (Y or N)	
Elevation of the top of the additional volume	fmsl	

I DDO IECT INFORMATION

II. DESIGN INFORMATION		
Surface Areas		
Area, temporary pool	29,454 ft <sup>2</sup>	
Area REQUIRED, permanent pool	20,850 ft <sup>2</sup>	
SA/DA ratio	4.60 (unitless)	<b></b>
Area PROVIDED, permanent pool, A <sub>perm_pool</sub>	24,331 ft <sup>2</sup>	OK
Area, bottom of 10ft vegetated shelf, A <sub>bot_shelf</sub>	19,141 ft <sup>2</sup>	
Area, sediment cleanout, top elevation (bottom of pond), $A_{bol\_pond}$	7,118 ft <sup>2</sup>	
Volumes	2	
Volume, temporary pool	33,134 ft <sup>3</sup>	OK
Volume, permanent pool, V <sub>perm_pool</sub>	83,897 ft <sup>3</sup>	
Volume, forebay (sum of forebays if more than one forebay)	19,013 ft <sup>3</sup> 22.7% %	Insufficient forchav volume
Forebay % of permanent pool volume	22.170 /0	Insufficient forebay volume.
SA/DA Table Data Design TSS removal	90 %	
Coastal SA/DA Table Used?	Y (Y or N)	
Mountain/Piedmont SA/DA Table Used?	N (Y or N)	
SA/DA ratio	4.60 (unitless)	
Average depth (used in SA/DA table):		
Calculation option 1 used? (See Figure 10-2b)	(Y or N)	
Volume, permanent pool, V <sub>perm_pool</sub>	ft <sup>3</sup>	
Area provided, permanent pool, A <sub>perm_pool</sub>	ft <sup>2</sup>	No. of 2 ft and a
Average depth calculated  Average depth used in SA/DA, d <sub>av</sub> , (Round to nearest 0.5ft)	ft ft	Need 3 ft min.
Calculation option 2 used? (See Figure 10-2b)	Y (Y or N)	
Area provided, permanent pool, A <sub>perm pool</sub>	24,331 ft <sup>2</sup>	
Area, bottom of 10ft vegetated shelf, A <sub>bot shelf</sub>	19,141 ft <sup>2</sup>	
Area, sediment cleanout, top elevation (bottom of pond), A <sub>bot pond</sub>	7,118 ft <sup>2</sup>	
	5.70 ft	
"Depth" (distance b/w bottom of 10ft shelf and top of sediment)  Average depth calculated	4.36 ft	OK
Average depth used in SA/DA, d <sub>av</sub> , (Round to nearest 0.5ft)	4.5 ft	OK
Drawdown Calculations		
Drawdown through orifice?	Y (Y or N)	
Diameter of orifice (if circular)	2.50 in	
Area of orifice (if-non-circular)	in <sup>2</sup>	
Coefficient of discharge (C <sub>D</sub> )	0.60 (unitless)	
Driving head (H <sub>o</sub> )	1.10 ft	
Drawdown through weir? Weir type	N (Y or N) (unitless)	
Coefficient of discharge (C <sub>w</sub> )	(unitless)	
Length of weir (L)	ft	
Driving head (H)	ft	
Pre-development 1-yr, 24-hr peak flow	25.66 ft <sup>3</sup> /sec	
Post-development 1-yr, 24-hr peak flow	26.61 ft <sup>3</sup> /sec	
Storage volume discharge rate (through discharge orifice or weir)	0.18 ft <sup>3</sup> /sec	
Storage volume drawdown time	2.10 days	OK, draws down in 2-5 days.
Additional Information		
Vegetated side slopes	3 :1	OK
Vegetated shelf slope	10:1	OK
Vegetated shelf width	10.0 ft	OK
Length of flowpath to width ratio  Length to width ratio	3 :1 2.8 :1	OK OK
Trash rack for overflow & orifice?	Y (Y or N)	OK OK
Freeboard provided	1.0 ft	OK
Vegetated filter provided?	N (Y or N)	OK
Recorded drainage easement provided?	Y (Y or N)	OK
Capures all runoff at ultimate build-out?	Y (Y or N)	OK
Drain mechanism for maintenance or emergencies is:	Pump	

### WK DICKSON

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### **VERTEX PHASE 1 – WET DETENTION POND #1**

AREA DRAINING TO POND =453,250 SF = 10.41 AC

IMPERVIOUS SURFACE AREA DRAINING TO POND:

IMPERVIOUS PAVEMENT = 22,755 SF

SIDEWALK = 0 SFBUILDING = 0 SF

> OTHER = 57,920 SF FUTURE = 68,724 SF

EXISTING IMPERVIOUS TO REMAIN = 114,394 SF

TOTAL = 263,793 SF

PERCENT IMPERVIOUS DRAINAGE AREA:

 $= (263,793 \text{ SF} / 453,250 \text{ SF}) \times 100$ 

= 58.2% **SAY 58%** 

POND DEPTH (FT)	SA/DA %	POND SURFACE AREA (MIN.) (SF)
4.50	4.6	20,850 SF

IF POND DEPTH = 4.50, MINIMUM SURFACE AREA = 20,850 SF

USED 90% TSS REMOVAL EFFICIENT IN COASTAL REGION CHART TO SIZE POND

AREA @ ELEVATION 40.2 = 24,331 SF > 20,850 SF

REQUIRED STORAGE FOR FOREBAY: 20% OF TOTAL PERMANENT POOL VOLUME

= (0.2)(83,897)

= 16,779 CF (19,013 CF PROVIDED)

**PROJECT:** Vertex Phase 1 **SUBJECT:** SW POND #1 CALCULATIONS **JOB NO.:** 20150016.00.WL **PREPARED BY:** WGB **DATE:** 10-1-15 **PAGE NO** 1 **OF** 3

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### **Pond Volume**

	Contour		Incremental	Curulative
	Elevation	Area	Volume	Volume
	(ft)	(sf)	(d)	(d)
BottomElevation	34.0	<i>7</i> 118	0	0
Battam of Shelf	39.7	19141	<i>7</i> 3056	<i>7</i> 3056
Permanent Pool	40.2	24331	10841	83897

### Forebay Volume

Contour		Incremental	Cumulative
Elevation	Area	Volume	Volume
(ft)	(sf)	(d)	(d)
34.0	924	0	0
39.7	4805	16328	16328
40.2	5936	2685	19013

**BottomElevation** Bottom of Shelf Permanent Pool

Forebay Volume is

of Pond Volume

PROJECT: Vertex Phase 1 SUBJECT: SW POND #1 CALCULATIONS JOB NO.: 20150016.00.WL **PREPARED BY:** WGB **DATE:** 10-1-15 **PAGE NO** 2 **OF** 3



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REQUIRED STORAGE FOR 1.5-INCH OF RUNOFF FOR POND: (use Simple Method)

Volume = 3630\*Rd\*Rv\*A

Rd = 1.5''

Rv = 0.05 + 0.9\*I = 0.05 + 0.9(0.582) = 0.5738

A = 453,250 SF / 43,560 Acre/SF = 10.41 Acres

Volume = 3630\*1.5"\*0.5738\*10.41 Acres

**= 32,510 CF** (33,134 CF PROVIDED)

**PROJECT:** Vertex Phase 1 **SUBJECT:** SW POND #1 CALCULATIONS **JOB NO.:** 20150016.00.WL **PREPARED BY:** WGB **DATE:** 10-1-15 **PAGE NO** 3 **OF** 3

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9/17/2015

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### INFILTRATION BASIN DRAWDOWN CALCULATIONS

1 Design Event: 1.5" Volume per Schueler's Method = 32510 C

2 Wet Detention Basin: Set Normal Bottom Elevation at SHW Elevation = 40.20

Contour			Cumulative
Elevation	Area	Volume	Volume
(FMSL)	(SF)	(CF)	(CF)
40.20	24331	0	0
40.70	27906	13048	13048
41.00	28566	8470	21518
42.00	30804	29675	51193
43.00	33097	31941	83134
44.00	35448	34262	117396

Water Surface Elevation for the 1.5" Volume =

41.4 EL

3 Wet Detention Basin Outlet:

2.5 " diameter orifice

Q = Cd\*A\*sqrt(2gh) =  $(0.6)(\pi(d/(2*12))^2)(sqrt(64.4*h))$ 

 $Q = (d^2/36.1)^* sqrt(h)$  cfs

4 Discharge from Wet Detention Pond to Infiltration Basin

Assume 1.5" Volume is Instantaneous

Orifice Head = h

$$h = 41.4-(40.2-((d/12)/2)) = 1.2-(d/24) = 1.1 in$$

Q = 0.18 cfs

Q = 0.18 cfs = 15,446 cf/day

Wet Detention Basin Release Time:

T = 1.5" Volume/Q (cf/day)

T = 2.10 days

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### 5 Infiltration Basin:

Bottom = 40.20 ELInfiltration Rate = 30 in/hr

Contour			Cumulative
Elevation	Area	Volume	Volume
(FMSL)	(SF)	(CF)	(CF)
40.20	15695	0	0
41.00	17779	13379	13379
42.00	20437	19091	32470
43.00	23152	21778	54248
44.00	25924	24522	78770

### 6 Infiltration Basin Release & Storage

### 1st Hour:

1.5 Volume = 32510 CF

Detention Basin Release Rate = 0.18 cfs

Volume to Infiltration Basin = 644 CF/hr or CF/1st hr

WSE Infiltration Basin = 40.24 EL Area at WSE = 15,795 SF

Qi = k(A)(h) = Q leaving the Infiltration Basin

Qi = 0.42 cfs

Qi = 0.42 cfs > Q = 0.18 cfs

### 1st 30 Minutes:

1.5 Volume = 32510 CF

Detention Basin Release Rate = 0.18 cfs

Volume to Infiltration Basin = 322 CF/30 mins

WSE Infiltration Basin = 40.22 EL

Area at WSE = 15,745 SF

Qi = k(A)(h) = Q leaving the Infiltration Basin

Qi = 0.21 cfs

Qi = 0.21 cfs > Q = 0.18 cfs

### **Vertex Railcar Corporation**

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Land Planning	qbw	9/17/2015	Wilmington, NC 28401
Surveying			(910) 762-4200

# Wet Detention Basin - Average Depth Calculation

Area Main Pond Area Forebay Total Area	924	1472	2076	10250 2738 12988	3455	4230	4805	0	0	0	0	0	0	28787	29009	29231	* L * C C
Elevation Area	34	35	36	37	38	39	39.7	40.2	40.7	41	42	43	44	41.1	41.2	41.3	
39.7	40.2	34		19141	24331	7118	5.7		0.45	3.91	4.36						
Elevation at Bottom of Shelf	Elevation at Permanent Pool	Elevation at Bottom of Pond		Area Bottom of Shelf	Area Permanent Pool	Area Bottom of Pond	Depth		Average Depth (1)	Average Depth (2)	Total Average Depth						

### Storm Sewers v10.40 Hydraflow Storm Sewers Extension for Autodesk® AutoCAD® Civil 3D® Plan Date: 10/1/2015 DI-7 DI-5 Number of lines: 4 <u>D</u>-4 Pipe - 3 Z. edla Pipe . 1 Project File: Proposed Storm WO Pond Outlets.stm

# Storm Sewer Inventory Report

0						
Line ID		Pipe - 2	Pipe - 3	Pipe - 1	Pipe - 4	Date: 10/1/2015
	Inlet/ Rim El (ft)	41.55	43.50	41.50	41.50	Date: 1
	J-Loss Coeff (K)	97.0	1.00	1.00	1.00	
	N Value (n)	0.011	0.011	0.011	0.011	
Data	Line Shape	Ö	Ċi	Ö	Ċ	f lines: 4
Physical Data	Line Size (in)	30	24	36	18	Number of lines: 4
	Invert EI Up (ft)	34.57	39.25	35.00	38.00	
	Line Slope (%)	0.25	3.17	06.0	2.33	
	Invert El Dn (ft)	34.00	36.76	34.00	34.00	
	Inlet Time (min)	5.0	5.0	5.0	5.0	
Data	Runoff Coeff (C)	08.0	0.80	08.0	08.0	
Flow Data	Drng Area (ac)	0.72	2.01	3.99	0.70	
	Known Q (cfs)	00.00	0.00	0.00	0.00	E
	Junc Type	DrCrb	DrCrb	DrCrb	DrCrb	Outlets.st
nent	Defl angle (deg)	-57.835	-26.628	-109.475 DrCrb	8.204	WO Pond
Alignment	Line Length (ft)	225.563	78.515	111.410	171.799	sed Storm
	Dnstr Line No.	End	~	End	End	Project File: Proposed Storm WO Pond Outlets.stm
Line		~	7	က	4	Project F

### Structure Report

Struct	Structure ID	Junction	Rim i		Structure			Line Out			Line In	
S		lype	Elev (ft)	Shape	Length (ft)	Width (ft)	Size (in)	Shape	Invert (ft)	Size (in)	Shape	Invert (ft)
~	DI-4	DropCurb	41.55	Rect	2.00	2.00	30	Oir	34.57	24	Cir	36.76
2	DI-5	DropCurb	43.50	Rect	2.00	2.00	24	Oir	39.25			
ო	DI-2	DropCurb	41.50	Rect	2.00	2.00	36	Öir	35.00			
4	DI-7	DropCurb	41.50	Rect	2.00	2.00	18	Öİ	38.00			
										-		
Project	Project File: Proposed Storm WO Pond Outlets.stm	d Outlets.stm					N	Number of Structures: 4	es: 4	Run E	Run Date: 10/1/2015	

# Storm Sewer Summary Report

	u						
	Junction Type	DropCurb	DropCurb	DropCurb	Dopourb	:015	
	Dns Line No.	End	<b>—</b>	End	End End	Run Date: 10/1/2015	
	HGL Junct (ft)	41.29	41.66	41.20	0. 	Run	-
	Minor loss (ft)	0.12	0.21	0.17	80 O		
	HGL Up (ft)	41.17*	41.44*	41.04*	4	lines: 4	
	HGL Down (ft)	40.94*	41.29*	40.94*	4 0.04 *	Number of lines: 4	
	Line Slope (%)	0.253	3.171	0.898	2.328		
	Invert EL Up (ft)	34.57	39.25	35.00	38·00 88·		
	Invert EL Dn (ft)	34.00	36.76	34.00	34.00		
	Line length (ft)	225.563	78.515	111.410	171.79		
	Line shape	Ö	Ċį	Ċį	ত <u>ঁ</u>		
· )	Line Size (in)	30	24	36	<del>6</del>		above crown
	Flow rate (cfs)	15.62	11.62	23.07	6. 6.	ıtlets.stm	arged (HGL
	Line ID	Pipe - 2	Pipe - 3	Pipe - 1	0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-	Project File: Proposed Storm WO Pond Outlets.stm	: Return period = 10 Yrs.; *Surcharged (HGL above crown).
	Line No.	~	7	ო	4	Project	NOTES:

### **Storm Sewer Tabulation**

	Grnd / Rim Elev Line ID	dn L	(ft)	36.88 41.55 Pipe - 2	41.55 43.50 Pipe - 3	37.42 41.50 Pipe - 1	35.79 41.50 Pipe - 4	
		Up Dn	(#) (#)	41.17 36	41.44	41.04 37	41.12 35	
	HGL Elev	Du	(ft)	40.94	41.29	40.94	40.94	
	lev	ď	(t)	34.57	39.25	35.00	38.00	
	Invert Elev	n D	(#)	34.00	36.76	34.00	34.00	
		Slope	(%)	0.25	3.17	0.90	2.33	
	Pipe	Size	(in)	30	24	36	18	
	Vel		(ft/s)	3.18	3.70	3.26	2.29	
	Cap	<b>5</b>	(cfs)	24.36	47.60	74.67	18.94	
	Total			15.62	11.62	23.07	4.05	
	Rain T		(in/hr) (cfs)	7.2				
	L C	Syst	(min)	5.4	5.0	5.0	5.0	
	ဍ	Inlet	(min)	5.0	5.0	5.0	5.0	
•	ပ	Total	_	2.18	1.61	3.19	0.56	
	Area x C	lucr		0.58	1.61	3.19	95.0	
	Rnoff		(c)	08.0	0.80	0.80	08.0	
		Total	(ac)	2.73	2.01	3.99	0.70	
	Drng Area	Incr	(ac)	0.72	2.01	3.99		
	Len		(#)	225.563 0.72	78.515	111.410 3.99	171.799 0.70	
		To		End 2	7	End 1	End 1	
	Station	Line	-	1	8	က	4	

NOTES:Intensity = 121.80 / (Inlet time + 23.50)  $^{\Lambda}$  0.84; Return period =Yrs. 10; c = cir e = ellip b = box

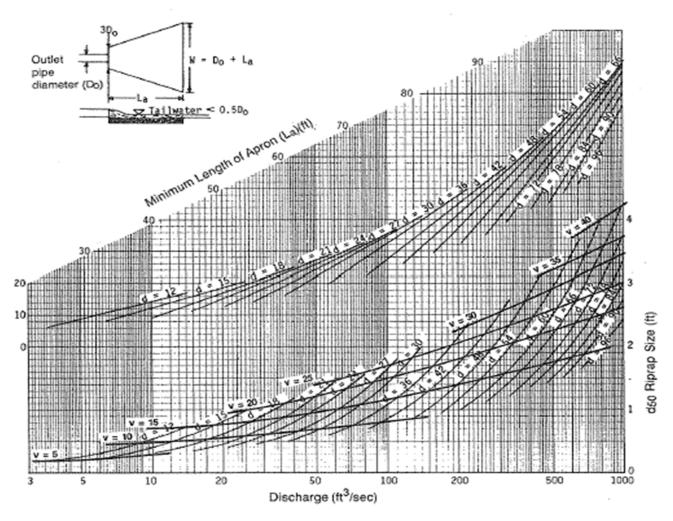
### Inlet Report

Byp	Š	# 0	) J	) J	JJ O	
	Depr (in)	0.0	0.0	0.0	0.0	
Inlet	Spread (ft)	278.45	1.#J	8303.64	263.65	Run Date: 10/1/2015
-	Depth (ft)	5.57	42.27	166.07	5.27	ın Date:
	Spread (ft)	278.45	1.#.1	8303.64 166.07	263.65	집
	Depth (ft)	5.57	42.27	166.07	5.27	
	c	0.013	0.013	0.013	0.013	4
Gutter	Sx (ft/ft)	0.020	0.000	0.020	0.020	Number of lines: 4
Ō	Sw (ft/ft)	0.020	0.000	0.020	0.020	Number
	× (£)	0.00	0.00	0.00	0.00	
	So (ft/ft)	Sag	Sag	Sag	Sag	
	× (f)	1.00	1.00	1.00	1.00	
Grate Inlet	(#)	1.00	1.00	1.00	1.00	
Gra	Area (sqft)	0.00	00.00	00.00	00.0	
let	(#)	1.00	1.00	1.00	1.00	
Curb Inlet	ťi)	4.0	4.0	4.0	0.4	
Junc	9 6	DrCrb	DrCrb	DrCrb	DrCrb	
Q	cfs)	0.00	0.00	0.00	0.00	
Q	(cfs)	4.16	11.62	23.07	4.05	ets.stm
Q	(cfs)	0.00	00:00	00:00	00.00	ond Outle
# Q	(cfs)	4.16	11.62	23.07	4.05	m WO Po
Inlet ID		DI-4	DI-5	DI-2	DI-7	Project File: Proposed Storm WO Pond Outlets.stm
Line	2	~	2	က	4	Projec

NOTES: Inlet N-Values = 0.016; Intensity = 121.80 / (Inlet time + 23.50) ^ 0.84; Return period = 10 Yrs.; \*Indicates Known Q added. All curb inlets are Horiz throat.

Vertex Railcar Co		tion
PROJECT NO.:2015001601WL DATE: 10/01/15	BY:	ETS
DATE: 10/01/15	T.M.:	WGB
REVISED: -	P.M.:	WGB

RIPRAP APRON DESIGN (NCDENR METHOD)



Design of outlet protection from a round pipe flowing full, minimum tailwater condition Tw<0.5 diameter

FES#	D <sub>o</sub> (Pipe ø)	T <sub>w</sub>	T <sub>w</sub> <0.5ø	Q	V	d <sub>50</sub>	L <sub>a</sub>	Apron width	Apron width	Max Stone	Apron
	(ft)	(ft)		(cfs)	(ft/s)	(ft)	(ft)	at pipe (ft)	at outlet (ft)	ø (ft)	Thickness(ft)
Stucture - 1	1.25	0	OKAY	6.68	5.44	0.25	9	3.75	10	0.38	0.56
Structure - 2	1.25	0	OKAY	6.68	5.44	0.25	9	3.75	10	0.38	0.56
Structure - 3	1.25	0	OKAY	6.68	5.44	0.25	9	3.75	10	0.38	0.56
FE-1	3	0	OKAY	23.07	3.26	0.5	22	9	25	0.75	1.13
FE-3	2.5	0	OKAY	15.62	3.18	0.5	20	7.5	23	0.75	1.13
FE-6	1.5	0	OKAY	4.05	2.29	0.25	11	4.5	13	0.38	0.56

Engineering Land Planning Surveying

wgb

909 Market Street 9/17/2015 Wilmington, NC 28401 (910) 762-4200

### Wet Detention Basin #1 Phase 1 and Ultimate Buildout Summary

Predeveloped CN				
Cover Type	Area (SF)	%	CN	Wtd. CN
Open Space (Poor)	221115	0.49	68	33.17
Gravel (Ballast)	6276	0.01	76	1.05
Impervious Area	225859	0.50	98	48.83
Total	453250			83.06
Composite CN 83.06			Use CN =	83

Postdeveloped CN				
Cover Type	Area (SF)	%	CN	Wtd. CN
Open Space (Poor)	188843	0.42	68	28.33
Gravel (Ballast)	21776	0.05	76	3.65
Impervious Area	242631	0.54	98	52.46
Total	453250			84.44
Composite CN 84.4	14	·	Use CN =	84

Storm Summary										
			Wet Basin	Infiltration						
24 Hr. Storm Event	Pre (cfs)	Post (cfs)	Routed (cfs)	Routed (cfs)						
1 Year	25.66	26.61	5.88	0						
2 Year	32.21	33.21	10.40	0						
10 Year	55.31	56.35	20.06	0						
25 Year	68.76	69.78	23.92	0						
100 Year	89.42	90.39	27.64	0						

Hydraflow Hydrographs Extension for AutoCAD® Civil 3D® 2015 by Autodesk, Inc. v10.4

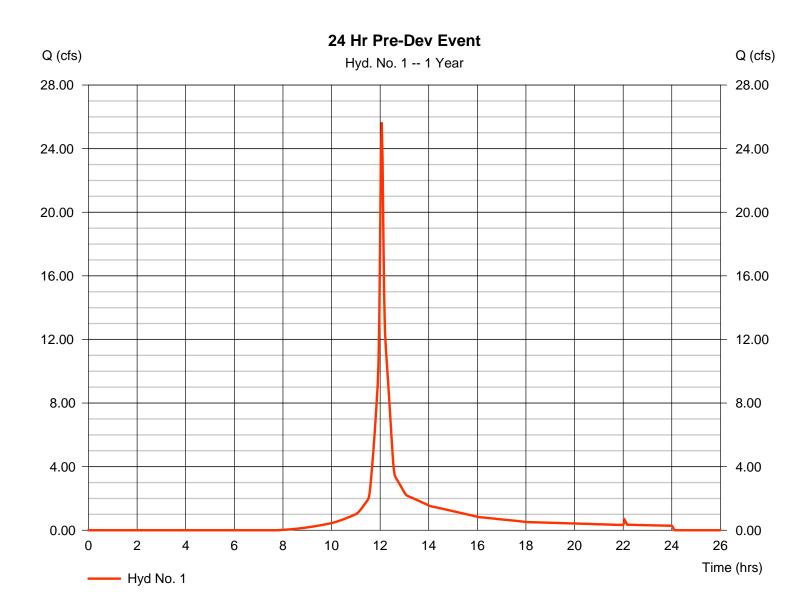
Wednesday, 09 / 30 / 2015

### Hyd. No. 1

24 Hr Pre-Dev Event

Hydrograph type = SCS Runoff Peak discharge = 25.66 cfsStorm frequency Time to peak = 12.07 hrs= 1 yrsTime interval = 2 min Hyd. volume = 76.702 cuftDrainage area Curve number = 10.410 ac= 83\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.86 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.080 x 68) + (5.190 x 98) + (0.140 x 76)] / 10.410



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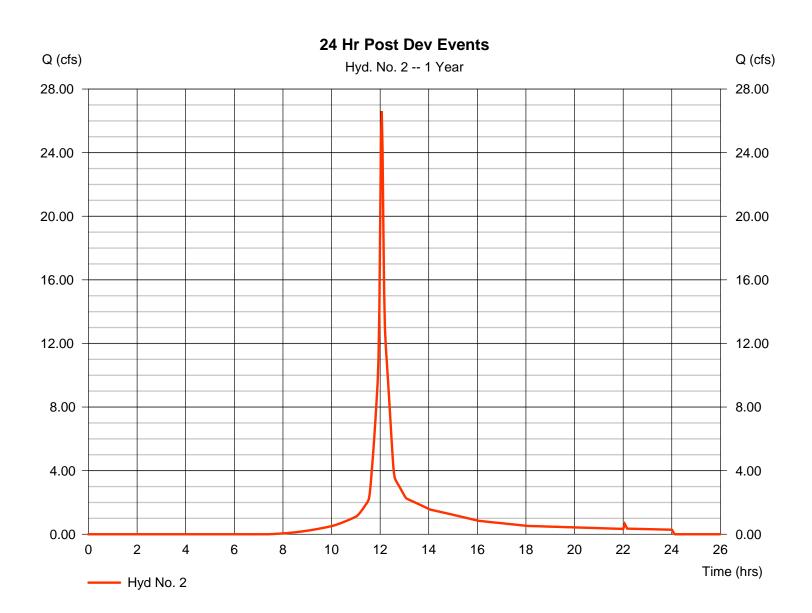
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### Hyd. No. 2

24 Hr Post Dev Events

Hydrograph type = SCS Runoff Peak discharge = 26.61 cfsStorm frequency Time to peak = 12.07 hrs= 1 yrsTime interval = 2 min Hyd. volume = 79.645 cuft Curve number Drainage area = 10.410 ac= 84\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 3.86 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.580 x 98) + (4.330 x 68) + (0.500 x 76)] / 10.410



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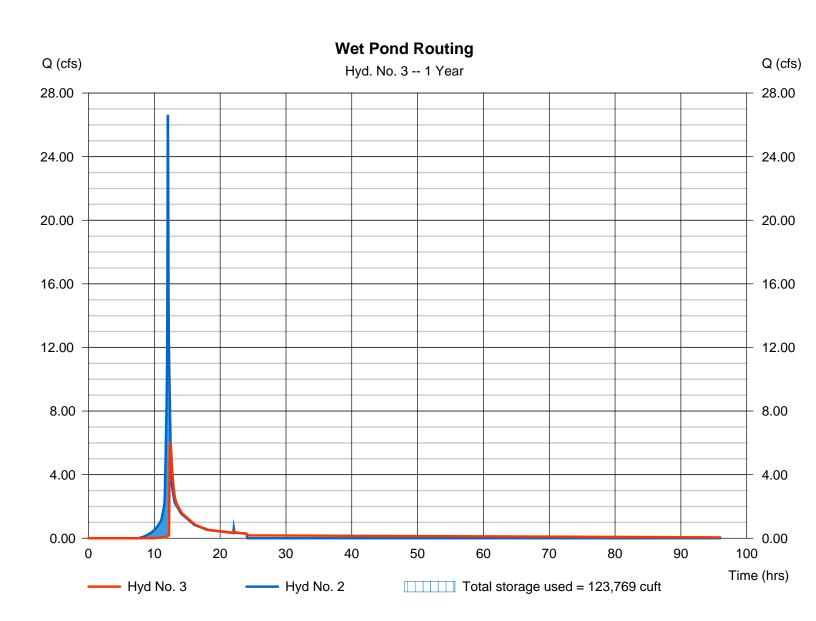
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### Hyd. No. 3

Wet Pond Routing

Hydrograph type = Reservoir Peak discharge = 5.882 cfsStorm frequency Time to peak  $= 12.47 \, hrs$ = 1 yrsTime interval = 2 min Hyd. volume = 74,038 cuftMax. Elevation Inflow hyd. No. = 2 - 24 Hr Post Dev Events = 41.62 ft= SW Pond #1 Reservoir name Max. Storage = 123,769 cuft

Storage Indication method used. Wet pond routing start elevation = 40.20 ft.



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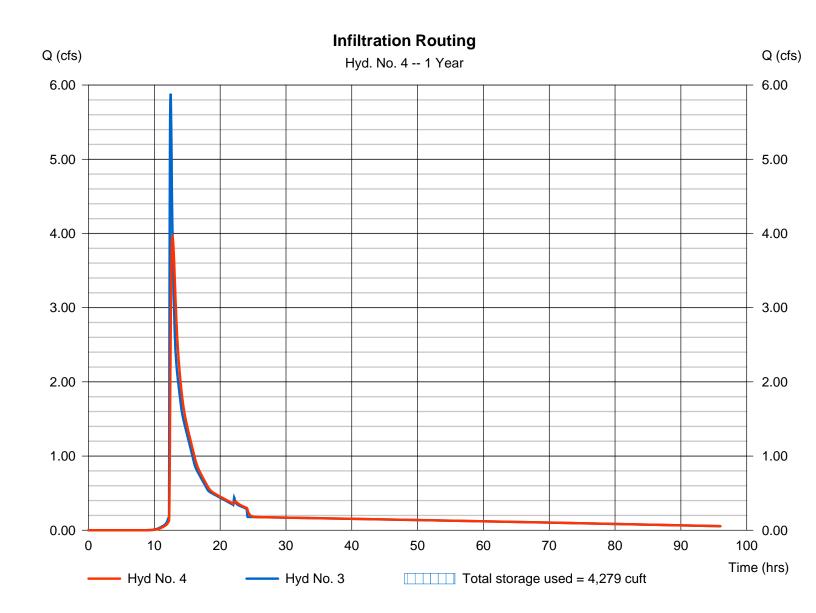
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### Hyd. No. 4

Infiltration Routing

Hydrograph type = Reservoir Peak discharge = 3.949 cfsStorm frequency Time to peak = 12.77 hrs= 1 yrsTime interval = 2 min Hyd. volume = 73,978 cuft Max. Elevation Inflow hyd. No. = 3 - Wet Pond Routing = 40.46 ft= Large Infiltration Basin Reservoir name Max. Storage = 4,279 cuft

Storage Indication method used. Outflow includes exfiltration.



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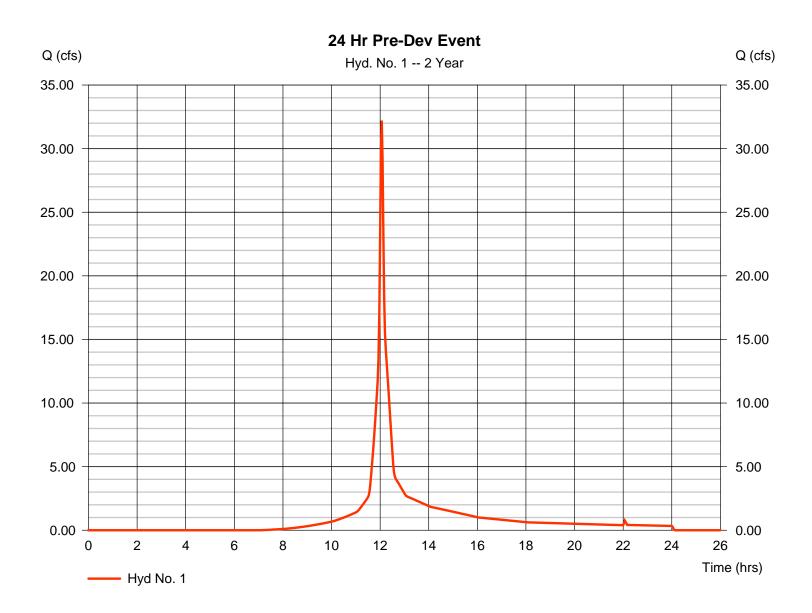
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### Hyd. No. 1

24 Hr Pre-Dev Event

Hydrograph type = SCS Runoff Peak discharge = 32.21 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 96.558 cuftDrainage area Curve number = 10.410 ac= 83\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 4.50 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.080 x 68) + (5.190 x 98) + (0.140 x 76)] / 10.410



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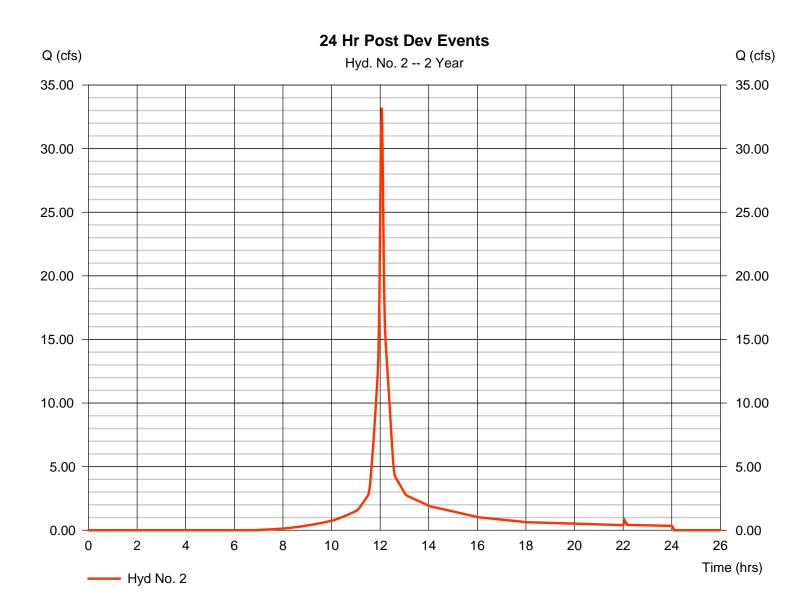
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### Hyd. No. 2

24 Hr Post Dev Events

Hydrograph type = SCS Runoff Peak discharge = 33.21 cfsStorm frequency = 2 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 99.782 cuftCurve number Drainage area = 10.410 ac= 84\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 4.50 inDistribution = Type III Storm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.580 x 98) + (4.330 x 68) + (0.500 x 76)] / 10.410



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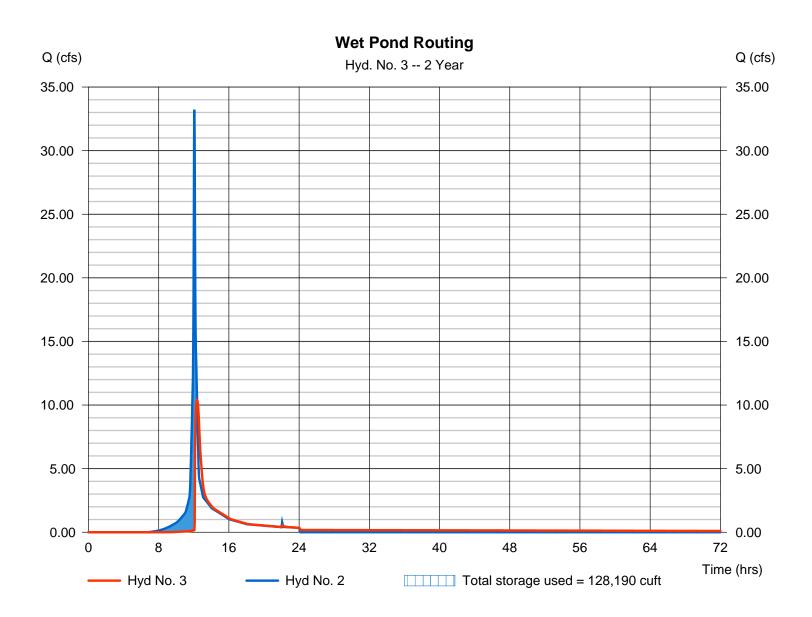
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### Hyd. No. 3

Wet Pond Routing

Hydrograph type = Reservoir Peak discharge = 10.40 cfsStorm frequency Time to peak = 12.37 hrs= 2 yrsTime interval = 2 min Hyd. volume = 94,168 cuft Max. Elevation Inflow hyd. No. = 2 - 24 Hr Post Dev Events = 41.77 ft= SW Pond #1 Reservoir name Max. Storage = 128,190 cuft

Storage Indication method used. Wet pond routing start elevation = 40.20 ft.



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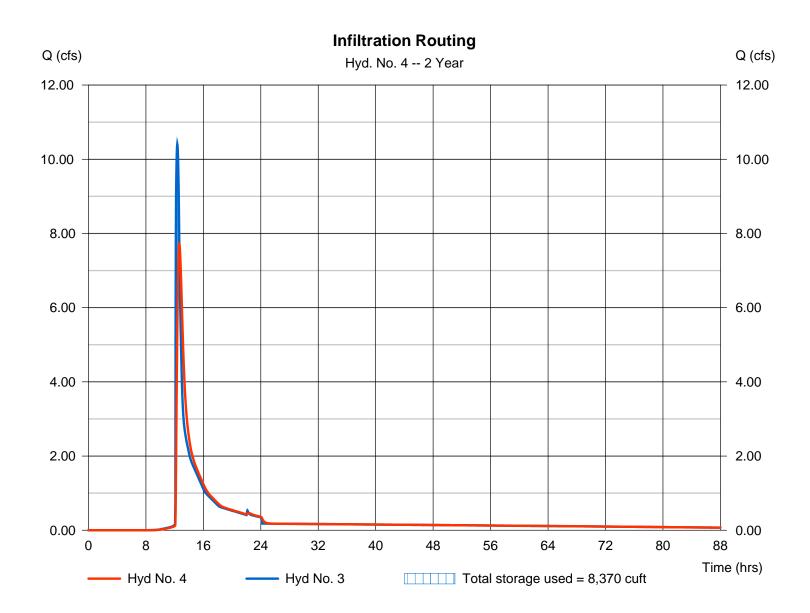
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### Hyd. No. 4

Infiltration Routing

Hydrograph type = Reservoir Peak discharge = 7.724 cfsStorm frequency Time to peak  $= 12.63 \, hrs$ = 2 yrsTime interval = 2 min Hyd. volume = 94,108 cuftMax. Elevation Inflow hyd. No. = 3 - Wet Pond Routing = 40.70 ftReservoir name = Large Infiltration Basin Max. Storage = 8,370 cuft

Storage Indication method used. Outflow includes exfiltration.



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= 484

### Hyd. No. 1

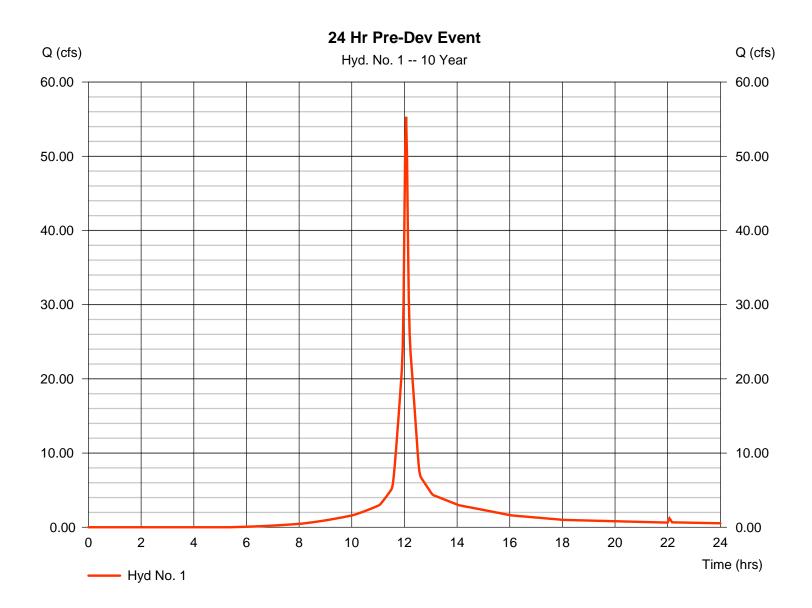
Storm duration

24 Hr Pre-Dev Event

= SCS Runoff Hydrograph type Peak discharge = 55.31 cfsStorm frequency = 10 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 168,774 cuftCurve number Drainage area = 10.410 ac= 83\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.72 inDistribution = Type III

Shape factor

= 24 hrs



<sup>\*</sup> Composite (Area/CN) = [(5.080 x 68) + (5.190 x 98) + (0.140 x 76)] / 10.410

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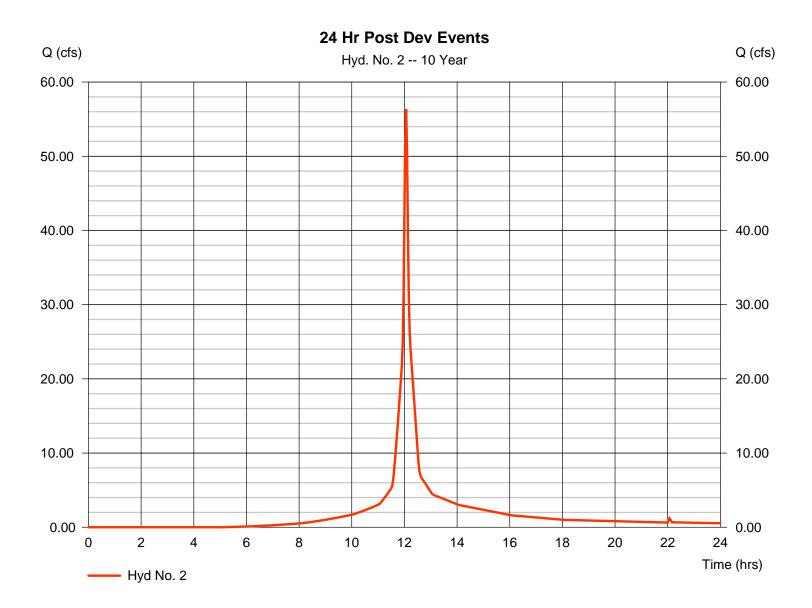
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### Hyd. No. 2

24 Hr Post Dev Events

Hydrograph type = SCS Runoff Peak discharge = 56.35 cfsStorm frequency = 10 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 172.683 cuft Curve number Drainage area = 10.410 ac= 84\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 6.72 inDistribution = Type III Shape factor Storm duration = 24 hrs = 484

<sup>\*</sup> Composite (Area/CN) = [(5.580 x 98) + (4.330 x 68) + (0.500 x 76)] / 10.410



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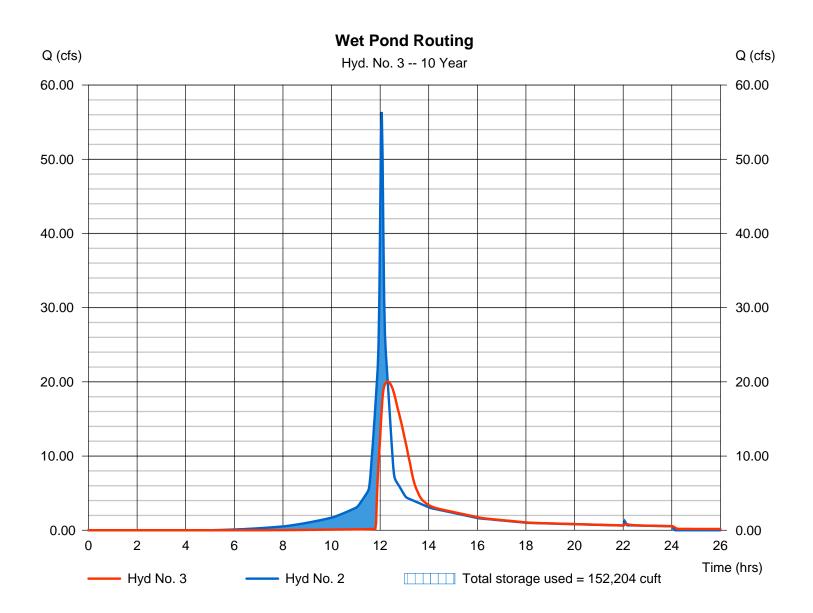
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### Hyd. No. 3

Wet Pond Routing

Hydrograph type = Reservoir Peak discharge = 20.06 cfsStorm frequency = 10 yrsTime to peak = 12.30 hrsTime interval = 2 minHyd. volume = 167,054 cuftMax. Elevation Inflow hyd. No. = 2 - 24 Hr Post Dev Events = 42.54 ft= SW Pond #1 Reservoir name Max. Storage = 152,204 cuft

Storage Indication method used. Wet pond routing start elevation = 40.20 ft.



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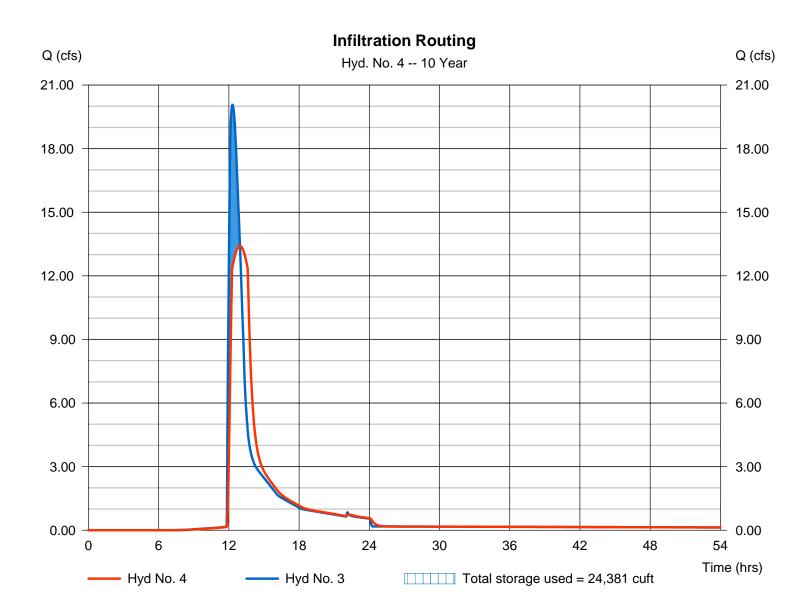
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### Hyd. No. 4

Infiltration Routing

Hydrograph type = Reservoir Peak discharge = 13.41 cfsStorm frequency = 10 yrsTime to peak  $= 12.93 \, hrs$ Time interval = 2 min Hyd. volume = 166,994 cuftMax. Elevation Inflow hyd. No. = 3 - Wet Pond Routing = 41.58 ftReservoir name = Large Infiltration Basin Max. Storage = 24,381 cuft

Storage Indication method used. Outflow includes exfiltration.



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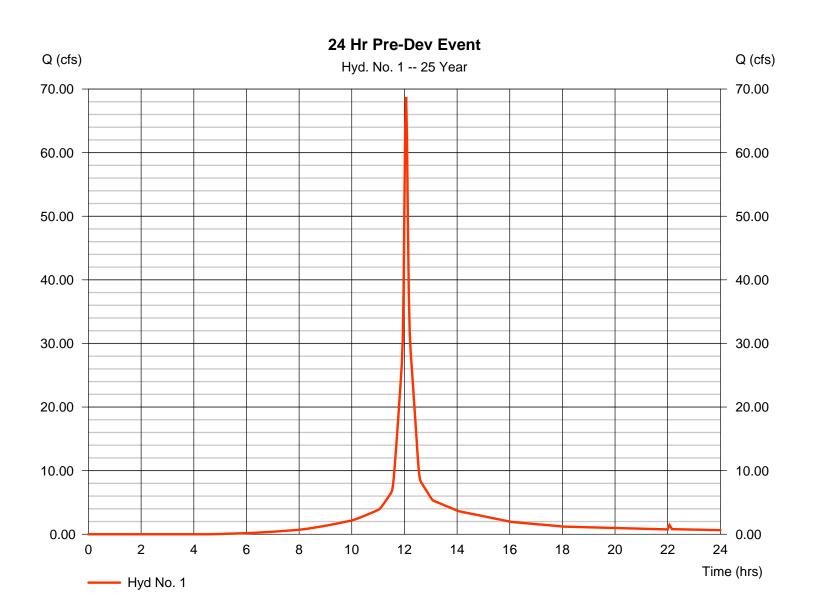
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### Hyd. No. 1

24 Hr Pre-Dev Event

= SCS Runoff Hydrograph type Peak discharge = 68.76 cfsStorm frequency = 25 yrsTime to peak = 12.07 hrsTime interval = 2 minHyd. volume = 212.097 cuft Drainage area Curve number = 10.410 ac= 83\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. Distribution = Type III = 8.01 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.080 x 68) + (5.190 x 98) + (0.140 x 76)] / 10.410



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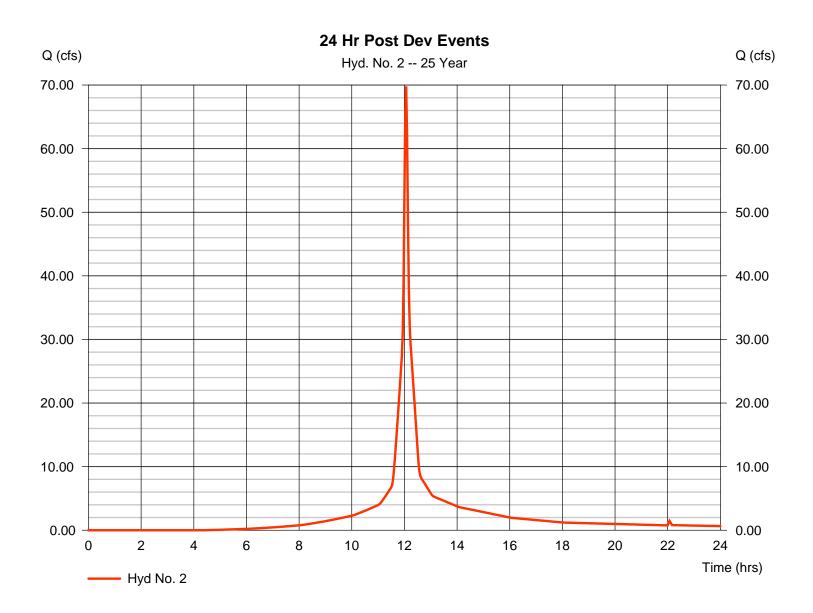
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### Hyd. No. 2

24 Hr Post Dev Events

Hydrograph type = SCS Runoff Peak discharge = 69.78 cfsStorm frequency = 25 yrsTime to peak = 12.07 hrsTime interval = 2 minHyd. volume = 216,273 cuftCurve number Drainage area = 10.410 ac= 84\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. Distribution = Type III = 8.01 inStorm duration = 24 hrs Shape factor = 484

<sup>\*</sup> Composite (Area/CN) = [(5.580 x 98) + (4.330 x 68) + (0.500 x 76)] / 10.410



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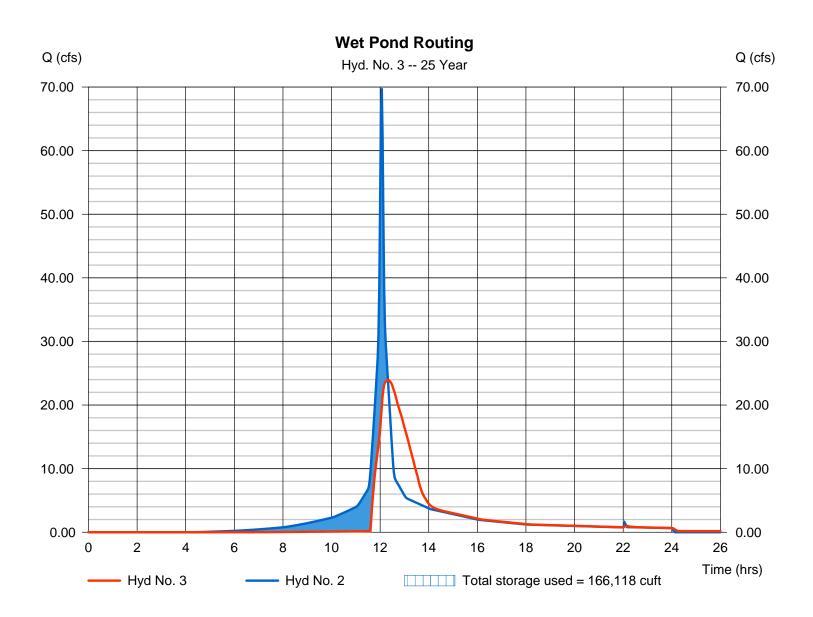
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### Hyd. No. 3

Wet Pond Routing

Hydrograph type = Reservoir Peak discharge = 23.92 cfsStorm frequency = 25 yrsTime to peak  $= 12.33 \, hrs$ Time interval = 2 minHyd. volume = 210,639 cuftMax. Elevation Inflow hyd. No. = 2 - 24 Hr Post Dev Events = 42.97 ft= SW Pond #1 Reservoir name Max. Storage = 166,118 cuft

Storage Indication method used. Wet pond routing start elevation = 40.20 ft.



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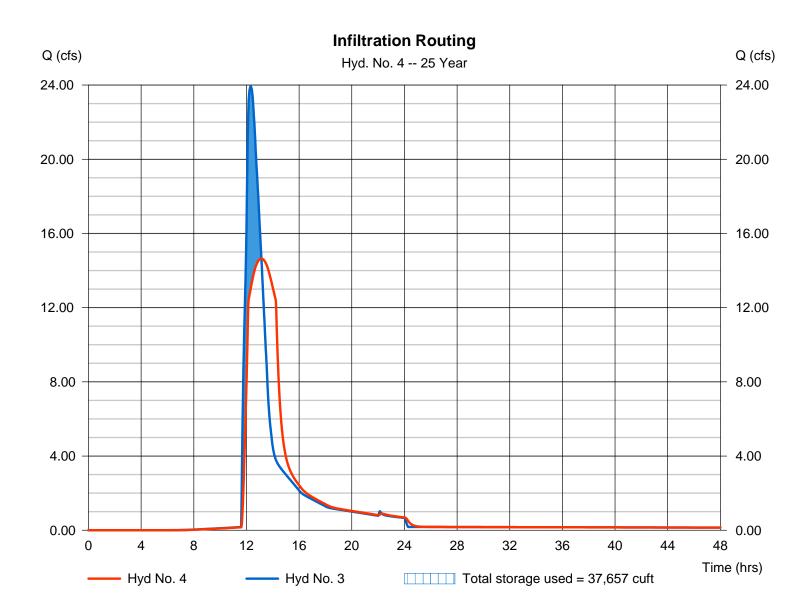
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### Hyd. No. 4

Infiltration Routing

Hydrograph type = Reservoir Peak discharge = 14.64 cfsStorm frequency = 25 yrsTime to peak  $= 13.13 \, hrs$ Time interval = 2 min Hyd. volume = 210,579 cuftMax. Elevation Inflow hyd. No. = 3 - Wet Pond Routing = 42.24 ftReservoir name = Large Infiltration Basin Max. Storage = 37,657 cuft

Storage Indication method used. Outflow includes exfiltration.



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= 484

### Hyd. No. 1

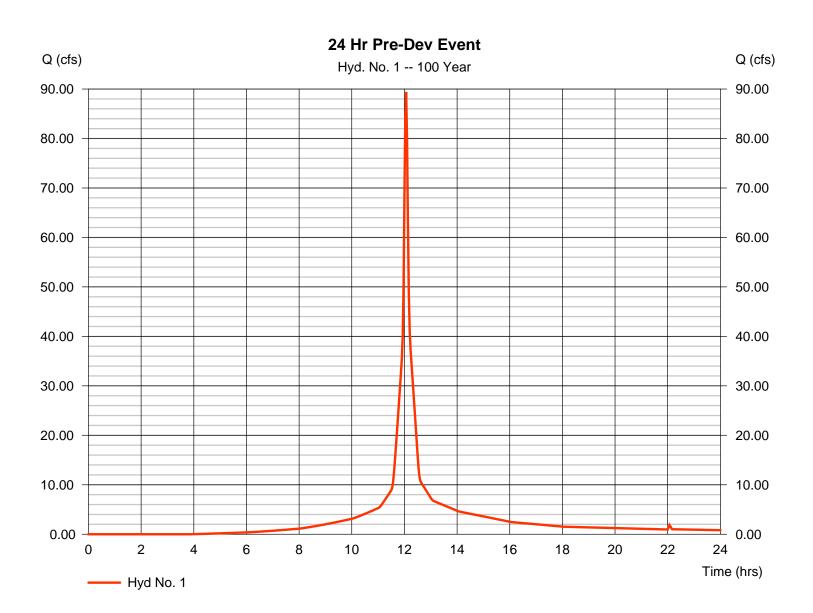
Storm duration

24 Hr Pre-Dev Event

Hydrograph type = SCS Runoff Peak discharge = 89.42 cfsStorm frequency = 100 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 279.962 cuft Curve number Drainage area = 10.410 ac= 83\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 10.00 inDistribution = Type III

Shape factor

= 24 hrs



<sup>\*</sup> Composite (Area/CN) =  $[(5.080 \times 68) + (5.190 \times 98) + (0.140 \times 76)] / 10.410$ 

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= 484

### Hyd. No. 2

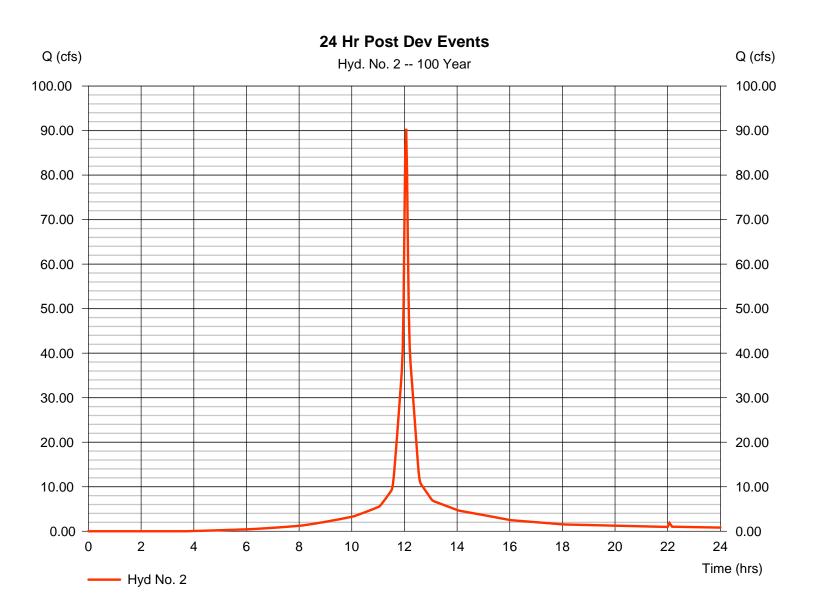
Storm duration

24 Hr Post Dev Events

Hydrograph type = SCS Runoff Peak discharge = 90.39 cfsStorm frequency = 100 yrsTime to peak = 12.07 hrsTime interval = 2 min Hyd. volume = 284.444 cuft = 10.410 acCurve number Drainage area = 84\*Basin Slope = 0.0 %Hydraulic length = 0 ftTc method Time of conc. (Tc)  $= 5.00 \, \text{min}$ = User Total precip. = 10.00 inDistribution = Type III

Shape factor

= 24 hrs



<sup>\*</sup> Composite (Area/CN) = [(5.580 x 98) + (4.330 x 68) + (0.500 x 76)] / 10.410

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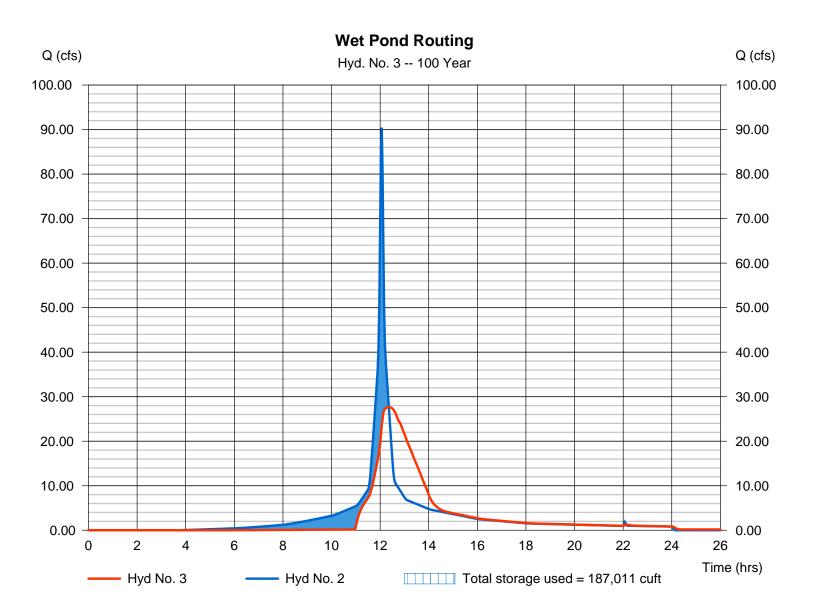
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### Hyd. No. 3

Wet Pond Routing

Hydrograph type = Reservoir Peak discharge = 27.64 cfsStorm frequency Time to peak = 12.37 hrs= 100 yrsTime interval = 2 minHyd. volume = 278,802 cuft Max. Elevation Inflow hyd. No. = 2 - 24 Hr Post Dev Events = 43.58 ft= SW Pond #1 Reservoir name Max. Storage = 187,011 cuft

Storage Indication method used. Wet pond routing start elevation = 40.20 ft.



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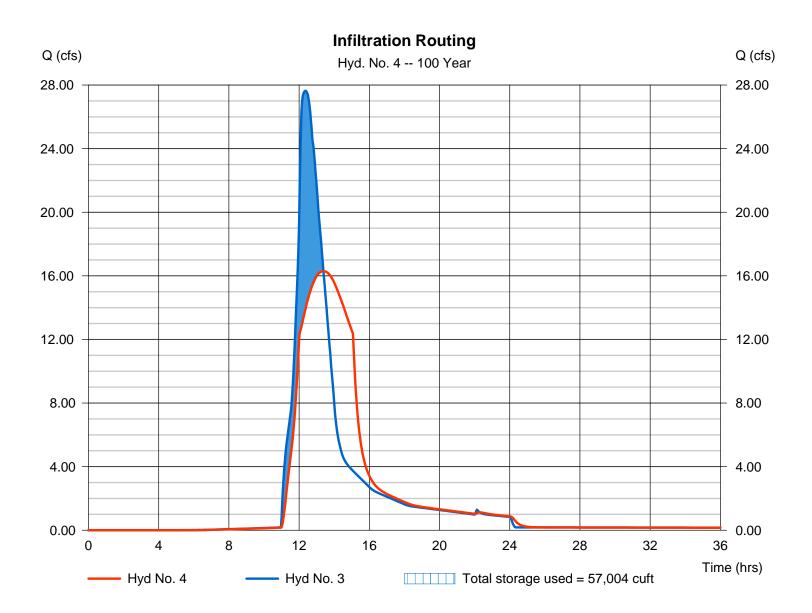
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### Hyd. No. 4

Infiltration Routing

Hydrograph type = Reservoir Peak discharge = 16.29 cfsStorm frequency Time to peak  $= 13.40 \, hrs$ = 100 yrsTime interval = 2 minHyd. volume = 278,742 cuft Max. Elevation Inflow hyd. No. = 3 - Wet Pond Routing = 43.11 ftReservoir name = Large Infiltration Basin Max. Storage = 57,004 cuft

Storage Indication method used. Outflow includes exfiltration.



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### Pond No. 1 - SW Pond #1

### **Pond Data**

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 34.00 ft

### Stage / Storage Table

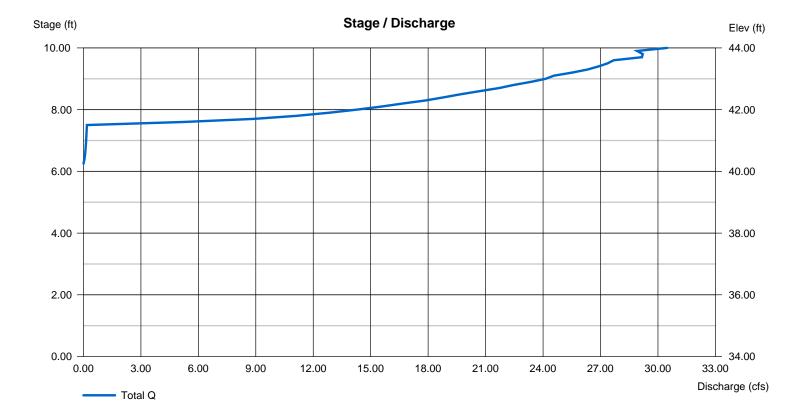
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	34.00	7,118	0	0
1.00	35.00	8,962	8,022	8,022
2.00	36.00	10,918	9,923	17,944
3.00	37.00	12,988	11,937	29,881
4.00	38.00	15,171	14,064	43,945
5.00	39.00	17,467	16,304	60,249
5.70	39.70	19,141	12,807	73,056
6.20	40.20	24,331	10,841	83,897
6.70	40.70	27,906	13,048	96,945
7.00	41.00	28,566	8,470	105,415
8.00	42.00	30,804	29,675	135,090
9.00	43.00	33,097	31,941	167,030
10.00	44.00	35,448	34,262	201,293

### **Culvert / Orifice Structures**

### **Weir Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	2.50	Inactive	0.00	Crest Len (ft)	= 16.00	16.00	16.00	0.00
Span (in)	= 15.00	2.50	0.00	0.00	Crest El. (ft)	= 41.50	41.50	41.50	0.00
No. Barrels	= 3	1	1	0	Weir Coeff.	= 3.33	3.33	3.33	2.60
Invert El. (ft)	= 40.20	40.20	0.00	0.00	Weir Type	= Broad	Broad	Broad	Broad
Length (ft)	= 35.00	0.00	0.00	0.00	Multi-Stage	= Yes	Yes	Yes	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (by	Wet area)		
Multi-Stage	= n/a	Yes	Yes	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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### Pond No. 4 - Large Infiltration Basin

### **Pond Data**

Contours -User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 40.20 ft

### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	40.20	15,694	0	0
0.80	41.00	17,779	13,379	13,379
1.80	42.00	20,437	19,091	32,470
2.80	43.00	23,152	21,778	54,248
3.80	44.00	25,924	24,522	78,771

### **Culvert / Orifice Structures Weir Structures** [A] [B] [C] [PrfRsr] [A] [B] [C] [D] Rise (in) = 0.000.00 0.00 Crest Len (ft) 0.00 0.00 0.00 0.00 = 0.00Span (in) = 0.000.00 0.00 0.00 Crest El. (ft) 0.00 0.00 0.00 = 0.00No. Barrels = 0 Weir Coeff. 0 0 = 3.333.33 3.33 3.33 Invert El. (ft) = 0.000.00 0.00 0.00 Weir Type = 0.000.00 0.00 0.00 Length (ft) Multi-Stage No No No = No n/a = 0.000.00 0.00 Slope (%) N-Value = .013.013 .013 n/a Orifice Coeff. 0.60 0.60 0.60 Exfil.(in/hr) = 0.60= 30.000 (by Contour) Multi-Stage = n/aNo No No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

